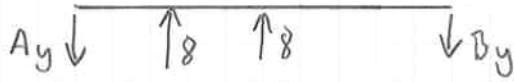


Mekanikkeksamen 24.02.2010 - Løsning

Oppg 1

a) FLD:



$$\overset{\sim}{\sum} M_A = 0 \Rightarrow B_y \cdot 5 - 8 \cdot 1,25 - 8 \cdot 2,5 = 0$$

$$\Rightarrow \underline{B_y = 6 \text{ kN}}$$

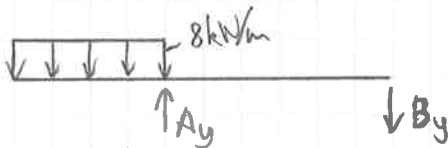
$$\uparrow \sum F_y = 0 \Rightarrow 8 + 8 - A_y - 6 = 0$$

$$\Rightarrow \underline{A_y = 10 \text{ kN}}$$

BD:



b) FLD:



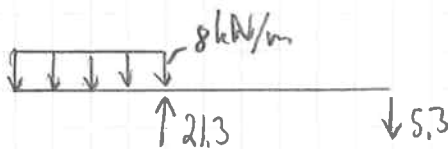
$$\overset{\sim}{\sum} M_A = 0 \Rightarrow B_y \cdot 3 - 8 \cdot 2 \cdot 1 = 0$$

$$\Rightarrow \underline{B_y = 5,3 \text{ kN}}$$

$$\uparrow \sum F_y = 0 \Rightarrow A_y - 5,3 - 8 \cdot 2 = 0$$

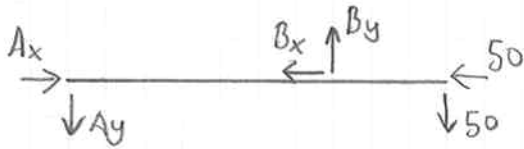
$$\Rightarrow \underline{A_y = 21,3 \text{ kN}}$$

BD:



Oppgave 2

a) FLD:



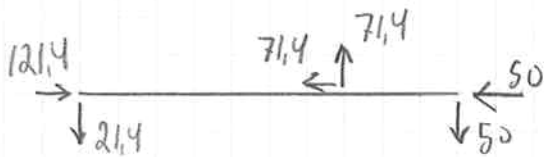
$$\sum \tilde{M}_A = 0 \Rightarrow 50 \cdot 5 - B_y \cdot 3,5 = 0 \Rightarrow \underline{B_y = 71,4 \text{ kN}}$$

Kraften i B har samme retning som staget (45°) og vi får $B_x = B_y$

$$\uparrow \sum F_y = 0 \Rightarrow 71,4 - 50 - A_y = 0 \Rightarrow \underline{A_y = 21,4 \text{ kN}}$$

$$\rightarrow \sum F_x = 0 \Rightarrow A_x - 71,4 - 50 = 0 \Rightarrow \underline{A_x = 121,4 \text{ kN}}$$

BD:



b)

$$A_{\text{stag}} = \frac{\pi}{4} 20^2 = 314 \text{ mm}^2$$

$$\text{Strålerkraft i stag: } T = \sqrt{B_x^2 + B_y^2} = \sqrt{2} B_x = \underline{101 \text{ kN}}$$

$$\underline{\underline{\sigma_{\text{stag}} = \frac{F}{A} = \frac{101000}{314} = 321,6 \text{ MPa}}}$$

$$L_{\text{stag}} = \sqrt{2} \cdot 3,5 = 4950 \text{ mm}$$

$$\underline{\underline{\Delta L = \frac{FL}{EA} = \frac{101000 \cdot 4950}{206000 \cdot 314} = 7,7 \text{ mm}}}$$

c)

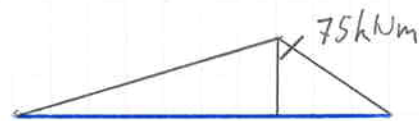
N-diagram :



V-diagram :



M-diagram :



d)

IPE 270 : $W_x = 429 \text{ cm}^3$

$A = 4590 \text{ mm}^2$

$$\sigma_{B0} = \frac{M_{dim}}{W_x} = \frac{75 \cdot 10^6}{429 \cdot 10^3} = 174,8 \text{ MPa}$$

$$\sigma_A = \frac{N}{A} = \frac{121400}{4590} = 26,4 \text{ MPa}$$

$$\underline{\underline{\sigma_{MAX}}} = \sigma_{B0} + \sigma_A = \underline{\underline{201,2 \text{ MPa}}}$$

$$\underline{\underline{n_F}} = \frac{235}{201,2} = \underline{\underline{1,17}}$$

e)



$$I_{\text{ent}} = 5790 - \frac{1}{12} \cdot 0,66 \cdot 5,0^3 = 5783 \text{ cm}^4$$

$$A_{\text{red}} = 4590 - 66 \cdot 50 = 4260 \text{ mm}^2$$

$$\sigma_{B0} = \frac{M}{I} y = \frac{75 \cdot 10^6}{5783 \cdot 10^8} \cdot \frac{270}{2} = 175,1 \text{ MPa}$$

$$\sigma_A = \frac{N}{A} = \frac{121400}{4260} = 28,5 \text{ MPa}$$

$$\underline{\underline{\sigma_{\text{max}} = \sigma_{B0} + \sigma_A = 203,6 \text{ MPa}}}$$

f)

$$A_{\text{steg}} = (270 - 50 - 2 \cdot 10,2) \cdot 6,6 = 1317 \text{ mm}^2$$

$$\tau = \frac{V}{A_s} = \frac{50 \cdot 10^3}{1317} = 38,0 \text{ MPa}$$

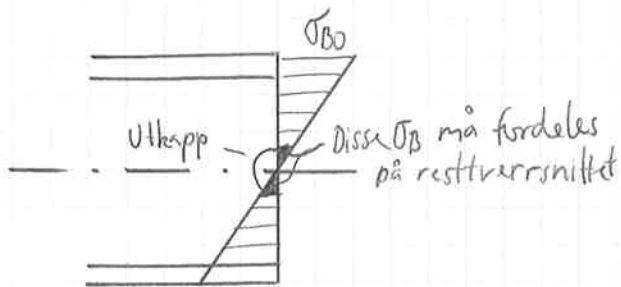
Berechner σ_B i steg et rett under flensen

$$\sigma_B = \frac{M y}{I_{\text{red}}} = \frac{75 \cdot 10^6}{5783 \cdot 10^6} \cdot (135 - 10,2) = 161,9 \text{ MPa}$$

$$\sigma = \sigma_B + \sigma_A = 161,9 + 28,5 = 190,4 \text{ MPa}$$

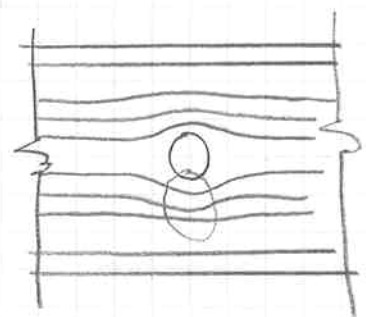
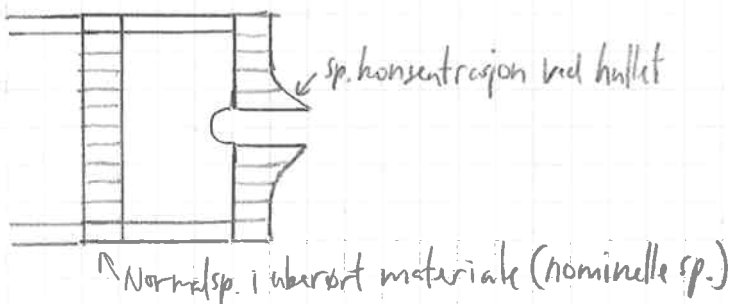
$$\underline{\underline{\sigma_j = \sqrt{\sigma^2 + 3\tau^2} = \sqrt{190,4^2 + 3 \cdot 38,0^2} = 201,4 \text{ MPa}}}$$

g) Hullet er plassert ved tverrsnittets nøytralakse hvor vi har små bøyespenninger og dermed blir det minimalt med bøyesp. som må fordeles på resttverrsnittet. Hvis utkippet ble gjort i flansen så ville spenningsbildet bli vesentlig forvirket



Utkippet vil ha en større innvirkning på aksialsp. og skjersp. Men som vi ser er σ_A og τ relativt små og av underordnet betydning i forhold til σ_B

Ved brå overganger i et tverrsnitts geometri (f.eks. ved utklipp) kan vi lokalt få svært store spenninger, og dette kalles spenningskonsentrasjonen. For å unngå dette bør vi unngå skarpe hjørner, plutselige dimensjonsendringer osv.



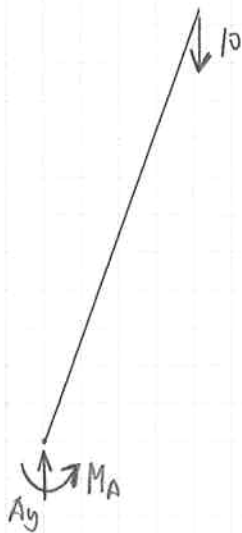
h)

$$F_k = \frac{\pi^2 EI_0}{lk^2} = \frac{\pi^2 \cdot 206000 \cdot 4200000}{3500^2} = 697 \text{ kN}$$

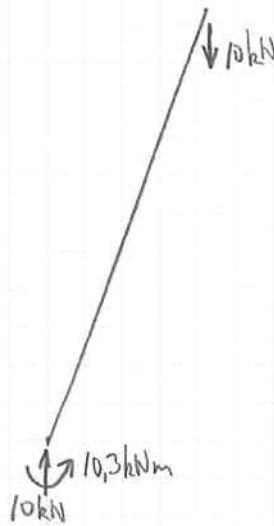
$$\underline{\underline{\frac{n_k}{k} = \frac{697}{121,4} = \underline{\underline{5,7}}}}$$

Oppgave 3

a) FLD:



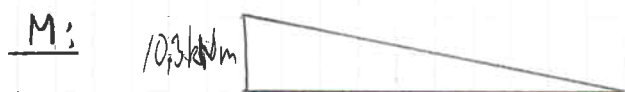
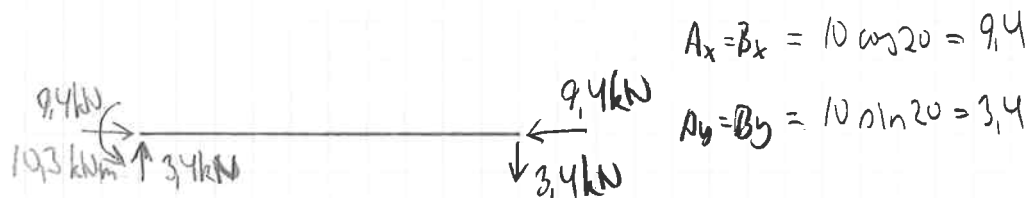
BD:



$$\uparrow \sum F_y = 0 \Rightarrow A_y = 10 \text{ kN}$$

$$\sum \overset{\curvearrowright}{M}_A = 0 \Rightarrow 10 \cdot 3 \cdot \sin 20 - M_A = 0 \Rightarrow M_A = 10,3 \text{ kNm}$$

b) Her er det en fordel i tegne et nyt BD hvor krefterne er dekomponert i bjelkeaksen og på tværs av bjelken. Ligger bjelken ned



c)

$$\sigma_{\text{tillatt}} = \frac{\sigma_F}{n} = \frac{235}{1.5} = 156.7 \text{ MPa}$$

$$W_{\text{tillatt}} = \frac{M_{\text{dim}}}{\sigma_{\text{tillatt}}} = \frac{10.3 \cdot 10^6}{156.7} = 65745 \text{ mm}^3 = 65.7 \text{ cm}^3$$

IPE140 har $W_x = 77.3 \text{ cm}^3$ og $A = 1640 \text{ mm}^2$

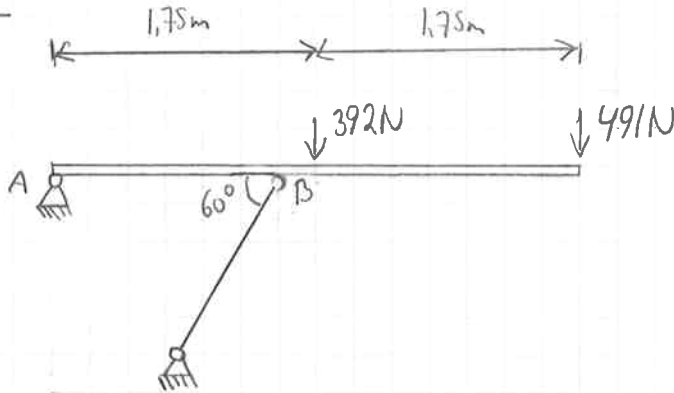
$$\sigma_B = \frac{10.3 \cdot 10^6}{77.3 \cdot 10^3} = 133.2 \text{ MPa}$$

$$\sigma_A = \frac{9400}{1640} = 5.7$$

$$\left. \begin{array}{l} \sigma_B = 133.2 \text{ MPa} \\ \sigma_A = 5.7 \end{array} \right\} \sigma = \sigma_B + \sigma_A = 138.9 \text{ MPa} < \sigma_{\text{tillatt}} \text{ dvs ok}$$

Oppgave 4

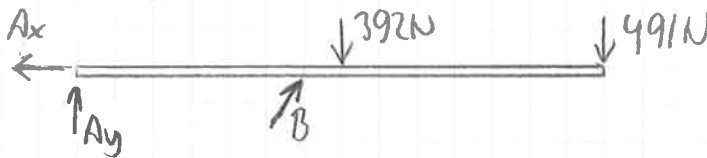
a) Modell:



$$F_{\text{person}} = 9.81 \cdot 50 = 491 \text{ N}$$

$$F_{\text{plinke}} = 9.81 \cdot 40 = 392 \text{ N}$$

FLO:



$$\begin{aligned} \sum \overset{\curvearrowright}{M}_A = 0 &\Rightarrow 392 \cdot 1.75 + 491 \cdot 3.5 - B \cdot \sin 60 \cdot 3.5 = 0 \\ &\Rightarrow \underline{B = 185 \text{ N}} \end{aligned}$$

b)

$$\uparrow \sum F_y = 0 \Rightarrow A_y + 185 \sin 60 - 392 - 491 = 0 \Rightarrow \underline{A_y = -720 \text{ N}}$$

$$\rightarrow \sum F_x = 0 \Rightarrow B \cos 60 - A_x = 0 \Rightarrow \underline{A_x = 925 \text{ N}}$$

Kraft som virker i A:

$$A = \sqrt{A_x^2 + A_y^2} = \sqrt{925^2 + 720^2} = \underline{1172 \text{ N}}$$

Kraftens retning i A:

$$\tan \varphi = \frac{A_y}{A_x} = \frac{720}{925} = 0.78 \Rightarrow \underline{\varphi = 37.9^\circ}$$

Det er motkraften som virker på boltene:

